

SPIRAL CURVES

A PRACTICAL SOLUTION

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Transition curves, also known as spiral curves, were used on Interstate Highways, County Roads and Railroads. Most of the public right of ways have been re-platted to eliminate the spirals on right of way but there still are a few to give the Land Surveyor a challenge.

This proposed solution deals with a railroad right of way in Rogers, Minnesota. The example was chosen because our survey involved two different plats and a boundary survey prepared by others. The spiral curve was either ignored or dealt with incorrectly. The tables used for the data are for highway spirals but the application is close enough to give a valid boundary for the survey. If data tables could be found that applied to railroad curves, the calculations and path to the solution would be very similar. The tables, formulas and calculations are from the book "Transition Curves for Highways" by the Federal Works Agency, published in 1940. Copies are available through Amazon.com for a very reasonable price.

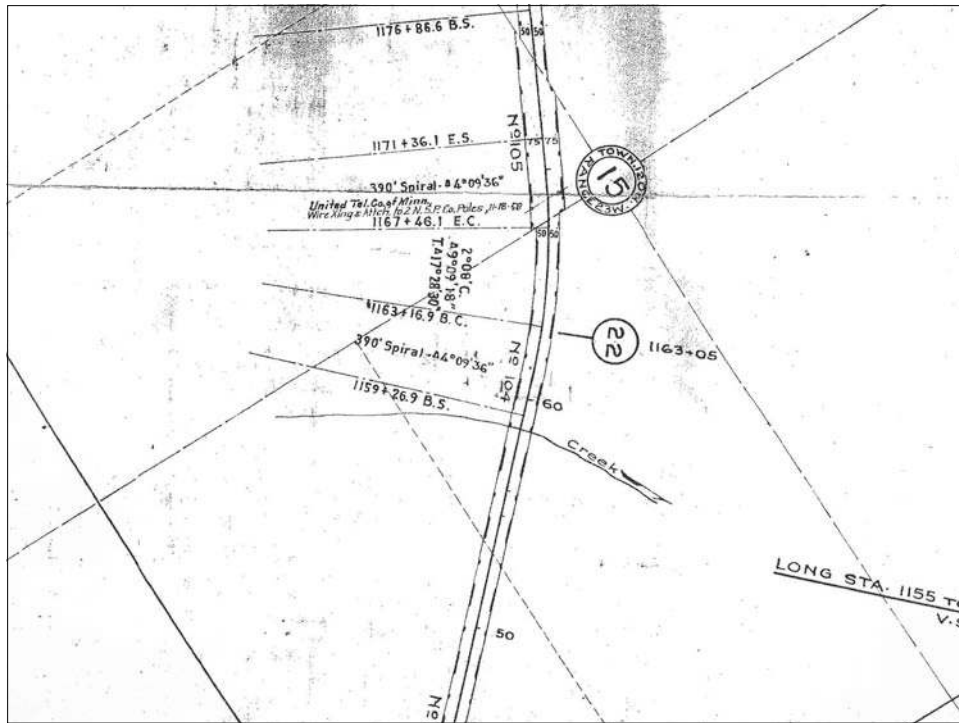
Transition Curves for Highways

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A normal spiral curve consists of three basic parts; the beginning spiral, a central circular curve and ending spiral. Whether working with a highway or a railroad, the right of way map or centerline description is needed. The minimum data necessary is the degree of curve, central angle of the circular curve, length of spiral and spiral central angle. From field measurements and a few calculations the spiral can be positioned.



Locate the center of track from about 500 feet before the curves to 500 feet beyond the curves. A shot every 50 feet through the curves will help to test the theoretical solution to the actual location of the tracks. Location of all found monuments and other physical objects should be included in the survey.

Calculated data needed to set up the curves include the central circular curve radius, circular curve central angle, circular curve tangent, spiral long tangent and spiral short tangents. See the typical curve drawing in the attached data.

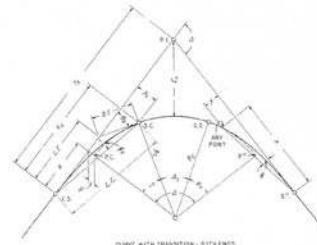
- k Distance from T.S. to point on tangent opposite the P.C. of the circular curve produced.
- Δ Intersection angle between tangents of entire curve.
- Δ_s Intersection angle between tangents at the S.C. and at the C.S. or the central angle of the circular curve portion of the curve.
- θ_s Intersection angle between the tangent of the complete curve and the tangent at the S.C., the spiral angle.
- θ Intersection angle between the tangent of the complete curve and the tangent at any other point on the spiral, the spiral angle of any other point.
- D_s Degree of the circular curve same as degree of curvature of spiral at the S.C. (arc definition).
- D Degree of curvature of spiral at any other point on spiral (arc definition).
- ϕ_s Deflection angle from tangent at T.S. to S.C.
- ϕ Deflection angle from tangent at any point on spiral to any other point on spiral.
- x_s, y_s Coordinates of S.C. from the T.S.
- x, y Coordinates of any other point on spiral from the T.S.

USE OF TABLES IN DESIGN

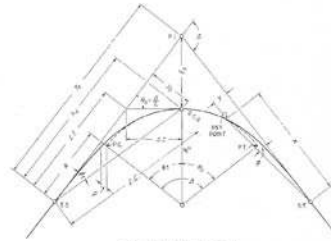
In designing highway alignment the angle between intersecting tangents is usually known as well as the limiting lengths of tangents and external distances.

Table IV gives tangent distances, T_s , and external distances, E_s , for numerous combinations of transition length, L_s , and degree of curvature, D_s . Each section of the table represents one value of the intersection angle Δ . All combinations above and to the right of a zigzag line are safe for the speed indicated at the end of the line. The designs that fit the limiting conditions of T_s or E_s , or both may be obtained directly from the table corresponding to the measured angle Δ .

After the combination of L_s and D_s is decided upon the value of T_s may be taken from the tables to the nearest hundredth of a foot and used to establish and locate the station of the T.S. by subtracting T_s from the station of the P.I. The central angle of the circular curve portion of the curve may be calculated by subtracting the central angle occupied by both transitions from the total central angle Δ . Thus $\Delta_c = \Delta - 2\theta_s = \Delta - \frac{L_s D_s}{100}$. Note that this is the only calculation required thus far and since L_s is always a multiple of 50 feet and D_s is in even degrees, except for values less than 4° when it is in even half



CURVE WITH TRANSITION - STRAIGHT



CURVE TRANSITIONAL THROUGHSIGHT
FIGURE 2.—Typical curves with transitions.

My assumption is that most surveyors will use cad software for the calculations. The solution can be tested manually. The method is in the above-mentioned book.

Use the field data to establish a best fit of the tangents running into and out of the curves. Intersect the tangents to determine P.I. of the curve set.

Determine the overall central angle for the curve set. The overall central angle will rarely match the plan angle. Adjust the difference in the circular curve and hold the spiral curve angles to the map or description angles.

Overall Central Angle	17 d 26' 06"
- Spiral Angle	-04 d 09' 36"
“	-04 d 09' 36"
Circular Central Angle	09 d 06' 54"

This application is for a rail line so the chord definition is used to calculate the radius of the circular curve.

$$\text{Radius} = 50 / \sin(2 \text{ d } 08' / 2) = 2685.89$$

Calculate the Tangent for the circular curve.

$$\text{Tangent} = 2685.89 * \tan(09 \text{ d } 06' 54'' / 2) = 214.11$$

All highway spirals are referred to as 10 chord spirals. The length is always a multiple of 50 feet. Railroad spirals do not hold to the length rule so their needs to be some interpolation of the tables to achieve a reasonable solution.

Use the tables to determine the Long Tangent and Short Tangent for a 390 foot spiral. Use the data for a 2d 00' curve or interpolate if the variation is large enough to make a difference.

$L_s = 350$ FT. TABLE V
FUNCTIONS OF TRANSITIONS
USED IN TABLE IV

D_c	θ_s	P	k	x_e	y_e	L.T.	S.T.	L.C.	D_c
1-30	0-00.8	1.233	174.99	0.0293	6.534	333.336	316.669	316.671	1-30
2-30	0-01.6	1.272	174.98	0.0587	5.133	333.338	316.671	316.671	2-30
3-30	0-02.4	1.311	174.97	0.0881	3.732	333.340	316.673	316.673	3-30
4-30	0-03.2	1.350	174.96	0.1175	2.331	333.342	316.675	316.675	4-30
5-30	0-04.0	1.389	174.95	0.1469	0.930	333.344	316.677	316.677	5-30
6-30	0-04.8	1.428	174.94	0.1763	0.529	333.346	316.679	316.679	6-30
7-30	0-05.6	1.467	174.93	0.2057	0.128	333.348	316.681	316.681	7-30
8-30	0-06.4	1.506	174.92	0.2351	0.027	333.350	316.683	316.683	8-30
9-30	0-07.2	1.545	174.91	0.2645	0.026	333.352	316.685	316.685	9-30
10-30	0-08.0	1.584	174.90	0.2939	0.025	333.354	316.687	316.687	10-30
11-30	0-08.8	1.623	174.89	0.3233	0.024	333.356	316.689	316.689	11-30
12-30	0-09.6	1.662	174.88	0.3527	0.023	333.358	316.691	316.691	12-30
13-30	0-10.4	1.701	174.87	0.3821	0.022	333.360	316.693	316.693	13-30
14-30	0-11.2	1.740	174.86	0.4115	0.021	333.362	316.695	316.695	14-30
15-30	0-12.0	1.779	174.85	0.4409	0.020	333.364	316.697	316.697	15-30
16-30	0-12.8	1.818	174.84	0.4703	0.019	333.366	316.699	316.699	16-30
17-30	0-13.6	1.857	174.83	0.5000	0.018	333.368	316.701	316.701	17-30
18-30	0-14.4	1.896	174.82	0.5294	0.017	333.370	316.703	316.703	18-30
19-30	0-15.2	1.935	174.81	0.5588	0.016	333.372	316.705	316.705	19-30
20-30	0-16.0	1.974	174.80	0.5882	0.015	333.374	316.707	316.707	20-30
21-30	0-16.8	2.013	174.79	0.6176	0.014	333.376	316.709	316.709	21-30
22-30	0-17.6	2.052	174.78	0.6470	0.013	333.378	316.711	316.711	22-30
23-30	0-18.4	2.091	174.77	0.6764	0.012	333.380	316.713	316.713	23-30
24-30	0-19.2	2.130	174.76	0.7058	0.011	333.382	316.715	316.715	24-30
25-30	0-20.0	2.169	174.75	0.7352	0.010	333.384	316.717	316.717	25-30

DEFLECTION ANGLES FROM T.S. TO POINTS
ON TEN CHORD SPIRAL FOR TRANSITIONS
USED IN TABLE IV

D_c	TRANSITION T.S. SIGHT ON POINT NO.										FOI	
	1	2	3	4	5	6	7	8	9	10-SC		
1-30	0-00.8	0-01.6	0-02.4	0-03.2	0-04.0	0-04.8	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6
2-30	0-01.6	0-02.4	0-03.2	0-04.0	0-04.8	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4
3-30	0-02.4	0-03.2	0-04.0	0-04.8	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2
4-30	0-03.2	0-04.0	0-04.8	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0
5-30	0-04.0	0-04.8	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8
6-30	0-04.8	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6
7-30	0-05.6	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4
8-30	0-06.4	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2
9-30	0-07.2	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0
10-30	0-08.0	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8
11-30	0-08.8	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6
12-30	0-09.6	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4
13-30	0-10.4	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2
14-30	0-11.2	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0
15-30	0-12.0	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8
16-30	0-12.8	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6
17-30	0-13.6	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4
18-30	0-14.4	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2
19-30	0-15.2	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0
20-30	0-16.0	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0	0-24.8
21-30	0-16.8	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0	0-24.8	0-25.6
22-30	0-17.6	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0	0-24.8	0-25.6	0-26.4
23-30	0-18.4	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0	0-24.8	0-25.6	0-26.4	0-27.2
24-30	0-19.2	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0	0-24.8	0-25.6	0-26.4	0-27.2	0-28.0
25-30	0-20.0	0-20.8	0-21.6	0-22.4	0-23.2	0-24.0	0-24.8	0-25.6	0-26.4	0-27.2	0-28.0	0-28.8

L = 400 FT. TABLE V
FUNCTIONS OF TRANSITIONS
USED IN TABLE IV

Dc	θs	p	k	Xc	Ye	Lt	St	Lc	Dc
1.00	3.0	1.74	189.94	392.89	6.08	246.71	133.37	286.55	1.00
2.00	4.0	2.32	199.47	399.83	9.30	268.73	133.40	299.51	2.00
3.00	5.0	2.81	199.93	399.73	11.63	286.77	133.43	309.46	3.00
4.00	6.0	3.21	199.93	399.56	13.95	301.82	133.47	319.40	4.00
5.00	7.0	3.53	199.93	399.35	16.26	314.87	133.50	329.35	5.00
6.00	8.0	3.78	199.93	399.10	18.56	325.92	133.53	339.30	6.00
7.00	9.0	4.00	199.93	398.81	20.85	335.97	133.56	349.25	7.00
8.00	10.0	4.19	199.93	398.49	23.13	345.02	133.59	359.20	8.00
9.00	11.0	4.36	199.93	398.14	25.40	353.07	133.62	369.15	9.00
10.00	12.0	4.51	199.93	397.77	27.66	360.12	133.65	379.10	10.00
11.00	13.0	4.64	199.93	397.38	29.91	366.17	133.68	389.05	11.00
12.00	14.0	4.76	199.93	396.97	32.15	371.22	133.71	399.00	12.00
13.00	15.0	4.87	199.93	396.54	34.38	376.27	133.74	408.95	13.00
14.00	16.0	4.97	199.93	396.09	36.60	381.32	133.77	418.90	14.00
15.00	17.0	5.07	199.93	395.62	38.81	386.37	133.80	428.85	15.00
16.00	18.0	5.16	199.93	395.14	41.01	391.42	133.83	438.80	16.00
17.00	19.0	5.24	199.93	394.65	43.20	396.47	133.86	448.75	17.00
18.00	20.0	5.32	199.93	394.14	45.38	401.52	133.89	458.70	18.00
19.00	21.0	5.39	199.93	393.62	47.55	406.57	133.92	468.65	19.00
20.00	22.0	5.46	199.93	393.09	49.71	411.62	133.95	478.60	20.00
21.00	23.0	5.53	199.93	392.55	51.86	416.67	133.98	488.55	21.00
22.00	24.0	5.59	199.93	392.00	54.00	421.72	134.01	498.50	22.00
23.00	25.0	5.65	199.93	391.45	56.13	426.77	134.04	508.45	23.00
24.00	26.0	5.71	199.93	390.89	58.25	431.82	134.07	518.40	24.00
25.00	27.0	5.76	199.93	390.33	60.36	436.87	134.10	528.35	25.00

Dc	1	2	3	4	5	6	7	8	9	10	SC	A	Dc
1.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	1.00
2.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	2.00
3.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	3.00
4.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	4.00
5.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	5.00
6.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	6.00
7.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	7.00
8.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	8.00
9.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	9.00
10.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	10.00
11.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	11.00
12.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	12.00
13.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	13.00
14.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	14.00
15.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	15.00
16.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	16.00
17.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	17.00
18.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	18.00
19.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	19.00
20.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	20.00
21.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	21.00
22.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	22.00
23.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	23.00
24.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	24.00
25.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	100.00	25.00

Short Tangent (ST) 350' Spiral 116.71

Short Tangent (ST) 400' Spiral 133.40

$$40/50 * (133.40 - 116.71) + 116.71 = 130.06$$

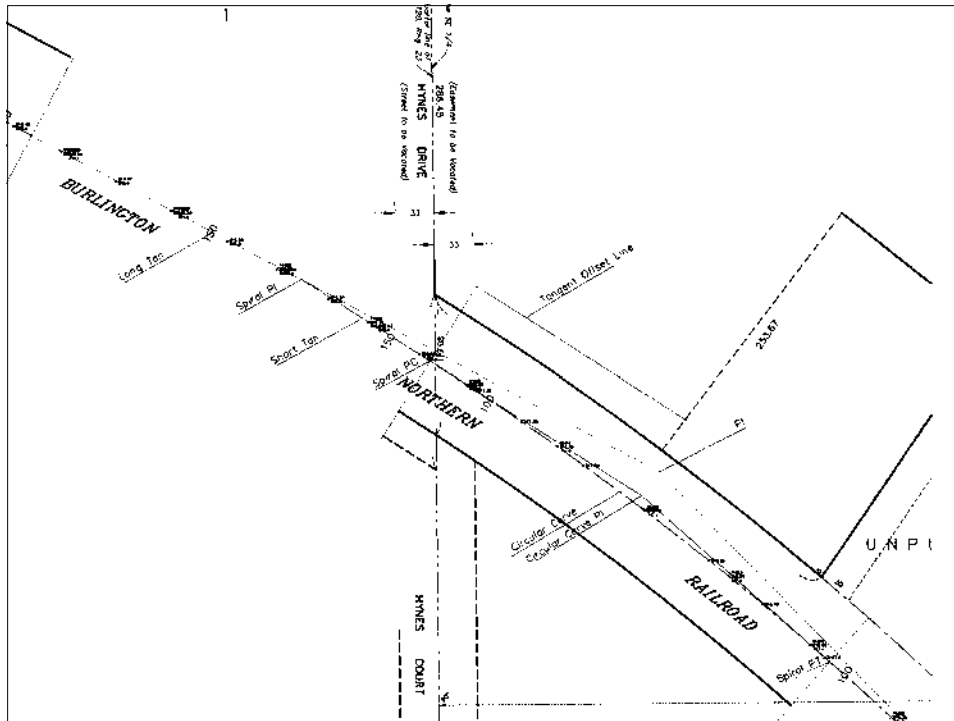
Long Tangent (LT) 350' Spiral 233.38

Long Tangent (LT) 400' Spiral 266.73

$$40/50 * (266.73 - 233.38) + 233.38 = 260.06$$

Off to the side in the cad software, use the tangent data and central angles to set up the curve tangents. Move the tangents onto the drawing, matching lines of the track centerline.

Extend radial lines to the right of way for the Begin Spiral, Spiral Circular Point (SC), Circular Spiral point (CS) and Spiral Tangent (ST).



Construct the spiral on centerline using cad.

- Curves and Lines
- Create Spirals
- Fit Tangent to Curve
- Select Tangent
- Select Curve

Zoom into the centerline to test the physical location of the tracks relative to the calculated curves. The expectation is that the mathematical solution should be within a few tenths of a foot of the actual location of the tracks. If there is a greater divergence, then the curves should be adjusted for a better fit.

Offset the Circular Curve to set the right of way.

There are two ways to establish the spiral curve on the right of way. The first, is to simply offset it the same as the circular curve. It's a reasonable solution and width checks through the curve indicate that is a parallel spiral. If the curve is measured using cad inquiry, the data returned is the same as centerline.

The second solution, is to use the method outlined above for the spiral on a centerline. The solution will give a different curve than the offset method and the width will also check properly. There will be some variation in the locations of the TS, SC, CS and ST. These positions can be adjusted by trimming and extending the curves to the original positions established by extending the radial lines. It is a good idea to calculate areas before trimming and adjusting the locations of the TS, SC, CS and ST.

The spiral curve data to be shown for the survey or plat should be the chord and chord bearing. The chord bearing and chord length can be measured directly from the location of the TS and SC. The Spiral Length is determined from the Table II - Functions of Transitions.

TABLE II - FUNCTIONS OF TRANSITION FOR L _s =1									
θ	p	k	α	y	L.T.	S.T.	L.C.	θ	
0.0	.0000	.5000	1.0000	.0000	.6667	.3333	1.0000	0.0	
.1	.015	.005	1.0000	.008	.67	.33	1.0000	.1	
.2	.029	.000	1.0000	.116	.67	.34	1.0000	.2	
.3	.044	.000	.9999	.175	.67	.34	1.0000	.3	
.4	.058	.000	.999	.233	.67	.34	1.0000	.4	
.5	.073	.000	.999	.291	.67	.34	1.0000	.5	
.6	.088	.000	.999	.349	.67	.34	1.0000	.6	
.7	.102	.000	.998	.407	.68	.34	.9999	.7	
.8	.117	.000	.998	.465	.68	.34	.9999	.8	
.9	.131	.000	.999	.524	.68	.34	.9999	.9	
1.0	.146	.000	.999	.582	.68	.34	.9999	1.0	
.1	.161	.999	.996	.640	.68	.35	.98	.1	
.2	.175	.999	.995	.698	.68	.35	.98	.2	
.3	.190	.999	.995	.756	.69	.35	.98	.3	
.4	.204	.999	.994	.814	.69	.35	.97	.4	
.5	.219	.999	.993	.873	.69	.36	.97	.5	
.6	.233	.999	.992	.931	.69	.36	.97	.6	
.7	.248	.998	.991	.989	.70	.36	.96	.7	
.8	.262	.998	.990	.1047	.70	.37	.96	.8	
.9	.277	.998	.989	.1105	.70	.37	.96	.9	
1.0	.292	.998	.988	.1163	.71	.37	.96	1.0	
2.0	.307	.998	.987	.1221	.71	.38	.96	2.0	
.1	.320	.997	.985	.1280	.72	.38	.93	.1	
.2	.334	.997	.984	.1338	.72	.39	.93	.2	
.3	.349	.997	.982	.1396	.72	.39	.92	.3	
.4	.363	.997	.981	.1454	.73	.39	.92	.4	
.5	.377	.996	.979	.1512	.74	.40	.91	.5	
.6	.392	.996	.978	.1571	.75	.40	.90	.6	
.7	.406	.996	.976	.1629	.75	.41	.90	.7	
.8	.421	.996	.975	.1687	.76	.41	.89	.8	
.9	.435	.995	.973	.1745	.76	.42	.89	.9	
1.0	.450	.995	.971	.1803	.77	.43	.87	1.0	
.1	.464	.994	.969	.1861	.78	.43	.86	.1	
.2	.479	.994	.967	.1919	.78	.44	.85	.2	
.3	.493	.994	.965	.1978	.79	.45	.84	.3	
.4	.508	.994	.963	.2036	.80	.45	.83	.4	
.5	.522	.993	.961	.2094	.81	.46	.82	.5	
.6	.537	.993	.959	.2152	.81	.47	.81	.6	
.7	.552	.993	.956	.2210	.82	.47	.80	.7	
.8	.566	.992	.954	.2268	.82	.48	.79	.8	
.9	.581	.992	.952	.2326	.83	.48	.78	.9	
1.0	.596	.991	.950	.2384	.83	.49	.77	1.0	
.1	.610	.991	.948	.2443	.84	.50	.76	.1	
.2	.625	.991	.946	.2501	.85	.51	.75	.2	
.3	.639	.990	.944	.2559	.85	.51	.74	.3	
.4	.654	.990	.942	.2617	.86	.52	.73	.4	
.5	.669	.989	.940	.2675	.86	.52	.72	.5	
.6	.683	.989	.938	.2733	.87	.53	.71	.6	
.7	.698	.989	.936	.2791	.87	.54	.70	.7	
.8	.712	.988	.934	.2849	.88	.54	.69	.8	
.9	.727	.988	.932	.2907	.88	.55	.68	.9	
1.0	.742	.987	.930	.2965	.89	.55	.67	1.0	
5.0	.3727	.4987	.9924	.02907	.66693	.33358	.99964	5.0	

FUNCTIONS OF TRANSITION FOR L _s =1 TABLE II 5°-10°									
θ	p	k	α	y	L.T.	S.T.	L.C.	θ	
5.0	.00727	.49877	.9924	.02907	.66693	.33358	.99964	5.0	
.1	.742	.987	.930	.2965	.89	.55	.67	.1	
.2	.756	.986	.928	.3023	.89	.56	.66	.2	
.3	.771	.986	.926	.3081	.89	.56	.65	.3	
.4	.785	.985	.924	.3139	.89	.57	.64	.4	
.5	.800	.985	.922	.3197	.89	.57	.63	.5	
.6	.814	.984	.920	.3255	.90	.58	.62	.6	
.7	.829	.984	.918	.3313	.90	.58	.61	.7	
.8	.843	.983	.916	.3371	.90	.59	.60	.8	
.9	.858	.983	.914	.3429	.90	.59	.59	.9	
6.0	.00872	.49882	.9919	.03488	.66705	.33368	.99951	6.0	
.1	.877	.981	.912	.3487	.90	.60	.58	.1	
.2	.891	.981	.910	.3545	.90	.60	.57	.2	
.3	.906	.980	.908	.3603	.90	.61	.56	.3	
.4	.920	.979	.906	.3661	.90	.61	.55	.4	
.5	.935	.979	.904	.3719	.90	.62	.54	.5	
.6	.949	.978	.902	.3777	.90	.62	.53	.6	
.7	.964	.977	.900	.3835	.90	.63	.52	.7	
.8	.978	.976	.898	.3893	.90	.63	.51	.8	
.9	.993	.975	.896	.3951	.90	.64	.50	.9	
7.0	.01018	.49975	.98851	.04068	.66719	.33381	.99934	7.0	
.1	.993	.974	.894	.4009	.90	.64	.49	.1	
.2	.1017	.973	.892	.4067	.90	.64	.48	.2	
.3	.1032	.972	.890	.4125	.90	.65	.47	.3	
.4	.1047	.971	.888	.4183	.90	.65	.46	.4	
.5	.1062	.970	.886	.4241	.90	.65	.45	.5	
.6	.1077	.969	.884	.4299	.90	.66	.44	.6	
.7	.1092	.968	.882	.4357	.90	.66	.43	.7	
.8	.1107	.967	.880	.4415	.90	.66	.42	.8	
.9	.1122	.966	.878	.4473	.90	.67	.41	.9	
8.0	.01143	.49967	.98805	.04648	.66735	.33395	.99913	8.0	
.1	.1137	.966	.876	.4531	.90	.67	.40	.1	
.2	.1152	.965	.874	.4589	.90	.67	.39	.2	
.3	.1167	.964	.872	.4647	.90	.68	.38	.3	
.4	.1182	.963	.870	.4705	.90	.68	.37	.4	
.5	.1197	.962	.868	.4763	.90	.68	.36	.5	
.6	.1212	.961	.866	.4821	.90	.69	.35	.6	
.7	.1227	.960	.864	.4879	.90	.69	.34	.7	
.8	.1242	.959	.862	.4937	.90	.69	.33	.8	
.9	.1257	.958	.860	.5000	.90	.70	.32	.9	
9.0	.01268	.49960	.98759	.05228	.66751	.33410	.99893	9.0	
.1	.1272	.958	.858	.5058	.90	.70	.31	.1	
.2	.1287	.957	.856	.5116	.90	.70	.30	.2	
.3	.1302	.956	.854	.5174	.90	.71	.29	.3	
.4	.1317	.955	.852	.5232	.90	.71	.28	.4	
.5	.1332	.954	.850	.5290	.90	.71	.27	.5	
.6	.1347	.953	.848	.5348	.90	.72	.26	.6	
.7	.1362	.952	.846	.5406	.90	.72	.25	.7	
.8	.1377	.951	.844	.5464	.90	.72	.24	.8	
.9	.1392	.950	.842	.5522	.90	.73	.23	.9	
10.0	.01413	.49949	.98696	.05808	.66773	.33420	.99865	10.0	

Spiral Central 4.1 d = LC 0.99977

Spiral Length = Chord / LC = 389.91/0.99977 = 390.00

Overall Spiral curve lengths on the right of way can be determined using the same equation. Arc lengths of sub-portions of spirals can't be determined using this method. For sub-portions of the spiral, show the Chord and Chord Bearing.

Calculating an area can be a problem with cad once the curves have been adjusted. There may be enough of a gap at the curve ends to cause the software to fail. A solution is to draw and use the chords to measure the area. There may need to be an adjustment for the area between the arc and chord.